

The key role of plant-wide modelling in wastewater treatment: experiences and challenges

A. Seco¹, MV Ruano^{1,*}, A. Ruiz-Martinez¹, A. Robles¹, R Barat², J. Serralta², J. Ferrer²

¹ CALAGUA Unidad Mixta UV-UPV, Department of Chemical Engineering, School of Engineering, Universitat de València. Av. Universitat s/n, 46100 Burjassot, Spain. Email: aurora.seco@uv.es, m.victoria.ruano@uv.es, ana.ruiz-martinez@uv.es, angel.robles@uv.es.

² CALAGUA Unidad Mixta UV-UPV, Research Institute of Water and Environmental Engineering, IIAMA. Universitat Politècnica de València. Camino de Vera s/n. 46022 Valencia Spain. Email: rababa@dihma.upv.es, jserralt@hma.upv.es, jferrer@hma.upv.es

*Corresponding author

Abstract: Plant-wide modelling can be considered an appropriate approach to represent the current complexity in water resource recovery facilities, reproducing all known phenomena in the different process units. Nonetheless, novel processes and new treatment schemes are still being developed and need to be fully incorporated in these models. This work presents a short chronological overview of some of the most relevant plant-wide models for wastewater treatment, as well as the authors' experience in plant-wide modelling using the general model BNRM, illustrating the key role of single plant-wide models in the field of wastewater treatment, both for engineering and research.

Keywords: Physico-chemical, chemical and biological processes; plant-wide modelling; water resource recovery; wastewater treatment

Introduction

Wastewater treatment modelling

In the wastewater treatment field, mathematical models are useful tools for research and development, as well as for design and optimization of the different processes involved. Mathematical modelling efforts are highly stimulated by different social, economic and environmental factors, such as the more and more stringent legislation, the urgent need of water recycling and carbon footprint reduction and the importance of general cost savings and public profile issues, among others. These factors force to move towards a more sustainable wastewater treatment design, where wastewater must turn into a source of resources such as reclaimed water, bioenergy and bioproducts (i.e. nutrients, biosolids). This paradigm shift requires the integration of sustainable processes in future water resource recovery facilities (WRRFs) (Batstone et al., 2015; Robles et al., 2018). In this respect, mathematical modelling plays a key role in the incorporation of the circular economy principles in the wastewater treatment sector.

Initially, wastewater treatment modelling focused on the biochemical processes taking place either on the water line or the sludge line. The ASM models (Henze et al., 2000) and the ADM1 model (Batstone et al., 2002) introduced the use of the Gujer or Petersen table (stoichiometric matrix) and are still today the most widely used tools for modelling activated sludge processes and anaerobic digestion (AD) processes, respectively. More recently, modelling efforts are focused on plant-wide modelling and aimed at simulating the whole plant, taking into account the effect of side-streams on mainstream. In this respect, a higher descriptive capacity of the whole wastewater treatment system can only be achieved if also physico-chemical and chemical processes are taken into account. For instance, a proper pH calculation has proven to

be necessary since it affects the stoichiometry and kinetics of biological (nitrification/denitrification) and chemical processes (phosphorus precipitation, gas solubility, etc.). Gas transfer processes also determine the effectivity of aeration, which involves a significant energy consumption and affects the carbon footprint estimation of WRRFs.

Plant-wide models

Plant-wide models have been developed following two different approaches: the interfaces approach and the general approach. The interfaces approach consists in connecting existing standard models by means of an interface between units and their models. Copp et al. (2003) and Nopens et al. (2009) defined ASM1-ADM1 interfaces, whereas Vanrolleghem et al. (2005) developed the Continuity-Based Model Interface Methodology (CBIM) proposing a procedure to connect any standard model. Dedicated tools have also been developed and widely adapted, such as the COST/IWA Benchmark Simulation Model No.1 (BSM1) (Copp 2002, Jeppsson and Pons 2004), the BSM1_LT (Rosen et al. 2004), the BSM2 (Jeppsson et al. 2006, Nopens et al. (2010)) and the BSM-MBR (Maere et al., 2011). They consist of a standardized simulation procedure for control strategies design in WWTP and their evaluation in terms of effluent quality and energy cost. The main advantage of using an interface-based approach with respect to other integrated methodologies is that the original model structure can be used, and there is thus no need for state variable representation in all process units with the resulting increased use of computational power, model complexity and adverse model stability characteristics (Grau et al., 2009).

On the other hand, the *general approach* makes use of a single model to describe the most relevant processes taking place in a WWTP. A single set of state variables is used, which includes the components of all processes involved. Therefore, aerobic, anaerobic and facultative microorganisms are considered in all treatment units and their growth will be determined by the environmental conditions. In this case, the user does not need to decide which model should be applied for each system. In general models there is a common characterization of the state of the process and the explicit calculation of pH is required as well. Although with higher computational costs, general models have become more and more feasible due to advances in computer technology. There are significant and successful single plant-wide models following the general approach in literature. For instance, the general Activated Sludge-Digestion models (ASDM) implemented in BioWin (EnviroSim Associates LTD) (Jones and Takács 2004), the Biological Nutrient Removal Model (BNRM) (Seco et al. 2004, Barat et al. 2013, Durán et al. 2017), the plant-wide modelling methodology proposed by Grau et al (2007), the plant-wide mass balance based steady-state WWTP model proposed by Ekama (2009) or the Mantis model incorporated in GPS-X software.

Current research on plant-wide models

As WRRFs increased in complexity, more complete and reliable plant-wide models are needed, able to reproduce the behaviour of the whole system. Novel processes are still being developed for water resource recovery (membrane-based processes, microalgae cultivation, etc.), but also mature and established technologies are being integrated in novel treatment schemes in order to achieve energy-positive WRRFs (Solon et al., 2019a). On the other hand, greater understanding in the hydrodynamics or the microbiological and biochemical fields have led to the development of the so-

called metabolic models (Lopez-Vazquez 2009) or CFD models (Rehman et al., 2017), respectively.

Currently, plant-wide modelling efforts are focused on integrating different model extensions to better reproduce the phenomena occurring in wastewater treatment and incorporate the new concepts and technologies that are emerging under the umbrella of circular economy. For instance, the last extensions of BSM2 are focused on modelling phosphorus plant-wide, a common goal within the scientific community mainly due to the issue of phosphate rock depletion. Flores-Alsina et al. (2015) proposed a plant-wide aqueous phase chemistry module describing pH variations and ion speciation/pairing in wastewater treatment process models whereas Kazadi Mbamba et al. (2016) developed a physico-chemistry framework. Afterward, Solon et al. (2017) integrated both extensions and also developed a new set of biological and physico-chemical process models to describe the required tri-phasic compound transformations and the close interlinks between phosphorus, sulphate and iron cycles. These extensions have been validated and then applied to optimize the chemical phosphorus removal in wastewater treatment systems (Kazadi Mbamba et al., 2019). On the other hand, the last extension of the single plant-wide model proposed by Grau et al. (2007) incorporated a physico-chemical plant wide framework (Lizarralde et al., 2015) which has been applied to optimize the phosphorus management strategies in Sur WWTP (Madrid, Spain) (Lizarralde et al., 2019) and to assess quantitatively the energy demand and resource recovery of different WRRF configurations (Fernández-Arévalo et al., 2017).

On the other hand, a plant-wide modelling approach which takes into account greenhouse gases (GHG) has become a common goal among researchers in the quest to reduce the carbon footprint of WRRFs (Mannina et al., 2016). Flores-Alsina et al. (2011) proposed a model called BSM2G which includes the estimation of the potential on-site and off-site sources of GHG emissions. This extension was then applied, for instance, to show the importance of adding GHG emissions as key performance evaluation criteria in WRRFs (Flores-Alsina et al. 2014). On the other hand, Mannina et al. (2019) proposed a plant-wide model for carbon and energy footprint which quantifies direct and indirect GHG emission related to biological and physical processes.

In summary, literature in the field shows an increasing and successful progress in plant-wide modelling, which can -and should- support the transition of WWTPs into WRRFs (Pretel et al., 2016b; Solon et al., 2019b), in order to facilitate water and nutrient recycling and carbon footprint reduction, but also general cost savings and compliance to new legislation. Table 1 shows a summary of the above presented plant-wide models, developed and applied during the last two decades.

Table 1: Mini review of some plant-wide models for wastewater treatment

Plant-wide model	References	Type
ASM1-ADM1 interfaces	Copp et al. 2003, Nopens et al. 2009	Interfaces
CBIM	Vanrolleghem et al. 2005	
BSM2	Jeppsson et al. 2006, Nopens et al. 2010	
BSM-MBR	Maere et al., 2011	
BSM2G	Flores-Alsina et al., 2011	
Extended BSM2 a plant-wide aqueous phase chemistry module describing pH variations and ion speciation/pairing	Flores-Alsina et al., 2015	
Extended BSM2 a modular physicochemistry framework (PCF)	Kazadi Mbamba et al., 2015	
Extended BSM2 from Flores-Alsina 2015 and Kazadi Mbamba 2015 and new set of biological and physico-chemical process models (P, Fe and S cycles)	Solon et al., 2017	
Optimisation of chemical phosphorus removal using extended BSM2 (Solon et al., 2017)	Kazadi Mbamba 2019	
Adding GHG emissions as key performance evaluation criteria in WRRFs using BSM2G	Flores-Alsina et al., 2014	
Mantis2 and its extension Mantis3	GPS-X (Hydromantis, Environmental Software Solutions Inc)	General
The general Activated Sludge-Digestion Model ASDM Implemented in BioWin®	EnviroSim Associates LTD	
Biological Nutrient Removal Model (No.1, No.2, No.2S)	Seco et al. 2004, Barat et al. 2013, Durán et al. 2017	
Plant-wide mass balance based steady-state WWTP model	Ekama 2009	
The plant-wide modelling methodology (PWM)	Grau et al., 2007	
Physico-chemical Plant Wide Modelling (PC-PWM) methodology for incorporating physico-chemical transformations into multiphase wastewater treatment process models	Lizarralde et al. 2015	
Optimization of the phosphorus management strategies in Sur WWTP using PC-PWM	Lizarralde et al. 2019	
Quantitatively assessment of the energy demand and resource recovery of WRRFs using PC-PWM	Fernández-Arévalo et al. 2017	
A plant-wide wastewater treatment plant model for carbon and energy footprint	Mannina et al. 2019	

Plant-wide modelling using BNRM

Model description

The Biological Nutrient Removal Model No.1 (BNRM1) for dynamic simulation of WWTPs was described by Seco et al. (2004). The physical, chemical and biological processes included were, respectively: settling and clarification processes (flocculated settling, hindered settling and thickening), volatile fatty acids elutriation and gas–liquid transfer; acid–base processes (equilibrium conditions are assumed); organic matter, nitrogen and phosphorus removal, acidogenesis, acetogenesis and methanogenesis. One of the most important advantages of this model was that no additional analysis with respect to ASM2d was required for wastewater characterization. Thus, the usual physiochemical parameters determined in a WWTP were enough to determine the model components.

However, this model did not consider nitrite and failed to accurately simulate the AD because precipitation processes were not considered. Therefore, an extension was proposed and named Biological Nutrient Removal Model No. 2 (BNRM2) (Barat et al. 2013). This extension comprised the components and processes required to simulate nitrogen removal via nitrite and the formation of the solids most likely to precipitate in anaerobic digesters (struvite, amorphous calcium phosphate, hydroxyapatite, newberite, vivianite, strengite, variscite, and calcium carbonate). Apart from nitrite oxidizing organisms (NOO), two groups of ammonium oxidizing organisms (AOO) were considered since different sets of kinetic parameters had been reported for the AOO present in activated sludge systems and SHARON (Single reactor system for High activity Ammonium Removal Over Nitrite) reactors.

The latest extension to the BNRM2, called BNRM2S, includes the activity of the sulphate reducing organisms (SRO) and was validated with a pilot-scale Anaerobic Membrane Bioreactor under steady-state and dynamic conditions (Durán et al. 2017).

The collection model BNRM is implemented in the simulation software DESASS (Ferrer et al., 2008) for steady-state and dynamic modelling. DESASS is linked with the geochemical model MINTEQA2 for equilibrium speciation calculations (Alison et al. 1991, EPA 2006). The solution procedure implemented in the software consists in a sequential iteration among the differential equations for the kinetic governed processes and the algebraic equations for the equilibrium governed processes. The section below “Full scale model applications” shows a compilation of experiences where the modelling results were obtained with this software, illustrating the potential of plant-wide modelling in research and development as well as in design of new plants or optimization of existing ones.

Wastewater characterization

Although the BNRM considers the most important physical, chemical and biological processes taking place in WWTPs, the required wastewater characterization is similar to the one for Activated Sludge Model No2d (Henze et al., 2000). Thus, the needed analyses are the following: COD (total and soluble fraction), BOD_{lim} (total and soluble fraction), Nitrogen (total and soluble fraction), ammonium, nitrite, nitrate, phosphorus (total and soluble fraction), orthophosphate, volatile fatty acids, pH, alkalinity and different ions such as sulphate, calcium, potassium and magnesium.

Model calibration

Accurate model predictions require a proper calibration of the model parameters. Model calibration can be carried out by fitting model predictions to dynamic experimental data (on-line calibration) or with laboratory experiments (off-line calibration). Due to the high number of parameters included in the BNRM, and given a set of experimental data, different sets of parameter values can be found able to reproduce the dynamic system performance. For this reason, it is recommended to identify the high influence model parameters (a small variation in these parameters leads to significant variations in model predictions) and to calibrate them with off-line laboratory experiments. For this purpose, *Penya-Roja et al. (2002)* developed an off-line calibration methodology for heterotrophic, autotrophic and polyphosphate accumulating organisms. The developed methodology consists in isolating specific processes for these bacterial groups and it is mainly based on Oxygen Uptake Rate (OUR) measurements. The methodology was upgraded by *Jimenez et al., 2011 and 2012* to estimate the model parameters related to the two bacterial groups involved in the nitrification process (AOB and NOB).

These kind of respirometric experiments provide information about the maximum bacterial activity under certain conditions, including biomass concentration of the different bacterial groups. In order to determine the maximum growth rate for each of these groups (in time^{-1} units) it is important to determine their concentration. *Borrás (2008)* developed a methodology to estimate the concentrations of PAO, GAO, AOB, NOB, methanogens and SRB in an activated sludge sample. This methodology is based on determining the percentage of viable bacteria (obtained by means of the LIVE/DEAD® BacLight™ Bacterial Viability Kit) and the percentage of each specific group over the whole bacteria using Fluorescent In-situ hybridization (FISH), a molecular cytogenetic technique. Knowing the suspended COD concentration of the sample, the concentration (in COD units) of each specific bacterial group can be estimated from the results obtained with the FISH.

Other specific calibration methodologies can be found in literature, such as that proposed by *Claros et al. (2011)* for AOB r-strategists, since it is known that the growth rate of AOB in a SHARON reactor (r-strategists species) depends on free ammonia (FA) concentration whereas the growth rate of AOB in activated sludge systems (k-strategists species) depends on total ammonium nitrogen (TAN) concentration. On the other hand, *Durán (2013)* developed an off-line procedure to calibrate the high influence parameters of other anaerobic microorganisms such as sulphate reducing bacteria.

Model validation

Different examples of BNRM validation can be found in literature. *Serralta et al., (2004)* demonstrated the model capability to predict the pH variations taking place in an A/O SBR system; *Barat et al., (2011)* showed the model capability to predict the variations in potassium, magnesium and calcium concentrations in an A/O SBR jointly with precipitation and redissolution processes; *Durán et al., (2017)* showed that the model was able to reproduce the performance of an AnMBR pilot plant (effluent composition, biomass wasted and biogas production) in different steady- and non-steady-state periods.

Full scale model applications

WWTP design, upgrade and optimization are among the most important applications of mathematical models in wastewater treatment. Mathematical models allow comparing the results obtained for different treatment schemes, different operating conditions, variable influent wastewater composition, etc. and therefore selecting the best alternative. The application of the BNRM to different full scale WWTPs is presented below. Examples are given of simulation results in quantitative (flows, concentrations, etc.) but also qualitative terms (development of strategies, schemes and decision support).

Design of a conventional WWTP

The BNRM was applied to design, according to the specified criteria, all the included elements for the public procurement process of a 100,000 m³/d WWTP in Sevilla (Spain). Simulations rendered information on dimensions of the different treatment units, effluent quality, aeration needs, sludge production, FeCl₃ needs, biogas production, NaOH and MgCl₂ addition for struvite recovery, as well as operational parameters for the activated sludge reactor and anaerobic digestion. An alternative solution to the proposed design criteria was also developed (Figure 1). This alternative solution was based on reducing sludge retention time (SRT), enhancing biological phosphorus removal, rearranging the sludge line to reduce uncontrolled precipitation problems and recovering phosphorus as struvite. A struvite crystallization unit was designed in order to recover the phosphorus from the reject water in the form of a slow-released fertilizer. Simulations results show that around 50% of the influent phosphorus would be recovered and 4.8 t/d of struvite would be produced.

Design of an AnMBR-based WWTP

The WWTP in Santa Rosa (Spain) was upgraded in 2016 with an AnMBR in order to demonstrate this technology as a sustainable alternative for sewage treatment. The plant was designed for treating 18 m³/d at ambient temperature: 15°C in winter and 25 °C in the summer season and with ground buried reactors. Modelling results under different operating and environmental conditions lead to the recommendation of operating at an SRT of 60 days, for which a biogas production depending on temperature was estimated: 1.34 or 1.70 m³/d was expected when operating at 15 or 25 °C, respectively. Methane yield resulted in ca. 160 and 200 STP L_{CH₄}/d at 15°C and 25°C, respectively. It is important to point out that sulphur concentration in the influent oscillated around 65 mg S/L, affecting therefore methanisation of organic matter due to the competition between Sulphate Reducing Organisms (SRO) and Methanogens, which could be reproduced by the model. The effluent quality parameters were also evaluated by simulation. The simulations revealed that the permeate could be used for fertigation purposes due to its ammonium and phosphate concentrations, while COD, BOD and SS were far below the discharge limits. Moreover, low amounts of waste sludge were achieved, being this sludge already stabilised. Specifically, 0.127 and 0.115 kg VSS per m³ of treated water were produced with a biodegradable volatile suspended solids (BVSS) content of 32.3 and 21.5% when operating at 15°C or 25°C, respectively. The application of the plant-wide model also allowed to predict the behaviour of the new plant in the events of polluting load increase or wastewater flow increase.

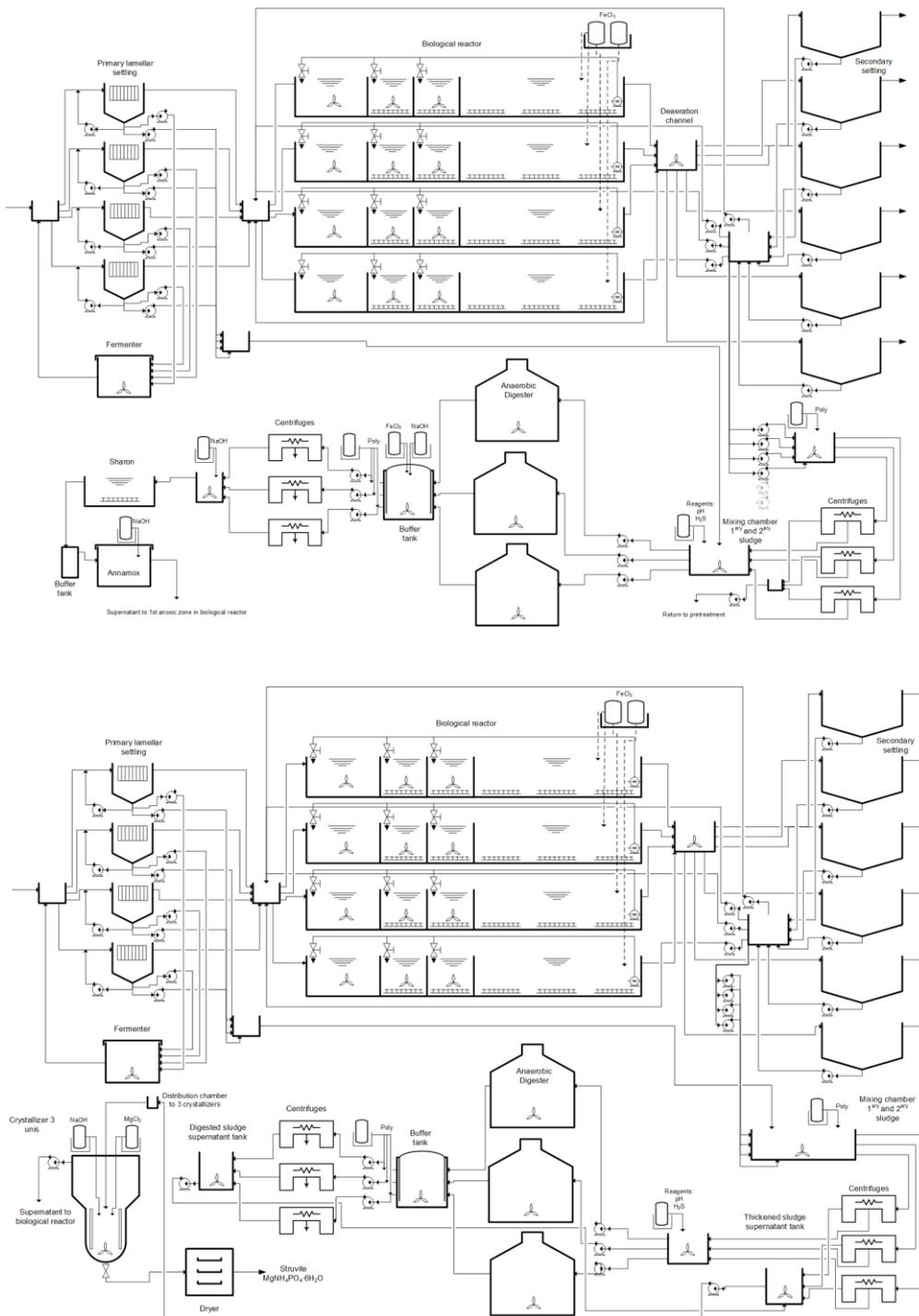


Figure 1: flow diagram of the base solution (above) and alternative solution (below)

Revamp of a WWTP by including an AnMBR

Currently, the urban WWTP in Torrent (Spain) cannot treat all the incoming wastewater flow and therefore a new installation needs to be built to increase the treatment capacity to 18,000 m³/d. Since agricultural activity in the area has a demand of 6,000 m³/d of water for irrigation an AnMBR system was deemed appropriate and therefore designed. The modelling results revealed the production of a high quality effluent, which complies with solids and organic matter content discharge limits and

presents nutrients concentrations for fertigation that allow for savings in the use of inorganic fertilizers. The effluent can be treated in the conventional activated sludge system in periods without agricultural need. The interconnection of the streams with a plant-wide model made it possible to simulate the whole system proposed.

Upgrade of a conventional WWTP

The plant-wide model was used to simulate different options for upgrading the Denia WWTP (Spain). This WWTP treats around 18,000 m³/d and was initially designed for organic matter removal and nitrification. The biological treatment consisted in a conventional activated sludge process whereas primary and excess sludge were aerobically digested. The decision to upgrade the WWTP was made in order to meet the EC requirements for total nitrogen and phosphorus in sensitive areas and solve the existing odour problems caused by the insufficient stabilization of the excess sludge. Different scenarios were simulated and the results used to support the decisions related to the WWTP upgrade. The modifications carried out in the treatment scheme consisted in: operation under extended aeration conditions, converting the biological reactors and the aerobic digesters in one plug-flow biological reactor, converting the old primary settlers into anoxic reactors and removing phosphorus by chemical precipitation. Moreover, simulations of significant ammonium and COD peak loads showed that increasing the anoxic zone would reduce sludge flotation problems. Therefore, an impeller was installed in the first part of the biological reactor to avoid suspended solids sedimentation when the air control valve was closed in order to increase the anoxic volume. The plant modifications proposed were successfully implemented (Seco et al. 2005).

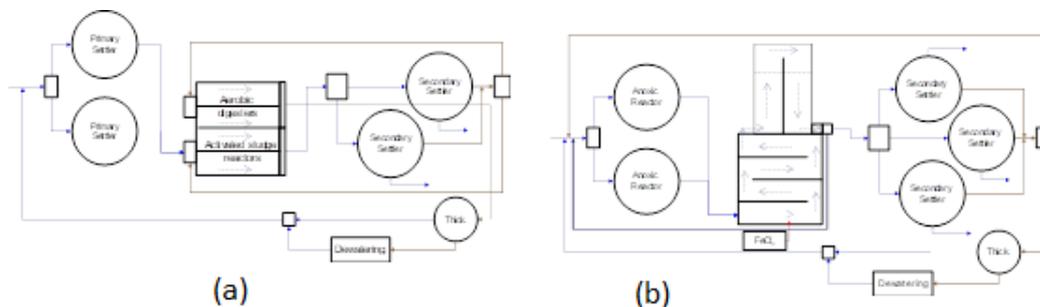


Figure 2: Treatment scheme of Denia WWTP a) Original b) Upgraded

Upgrade of a conventional WWTP for stream management

In WWTP with biological P removal it becomes very interesting to enhance P recovery and minimize uncontrolled P precipitation. For this, a modification in the sludge line was proposed after a simulation study and tested in different full scale applications (Tarragona, Calahorra and Murcia-Este WWTPs). The simulations evaluated the potential P recovery by mixing the thickened sludges under anaerobic conditions in a mixing chamber and pumping the mix towards the primary thickener, therefore obtaining an overflow stream highly enriched in orthophosphate available for its recovery. Figure 3a shows the schematic description of the sludge line configuration and Figure 3b shows concentration of orthophosphate in the overflow stream, estimated at different operational conditions in Murcia-Este WWTP. The details of the simulation and optimization work in the Tarragona WWTP can be found in Ruano et al. 2012 whereas Martí et al. 2017 describe the case of Calahorra WWTP.

This configuration allows to recover up to 40% of the incoming phosphorus and considerably reduces the uncontrolled phosphorus precipitation in digesters, pipes, centrifuges and other equipment.

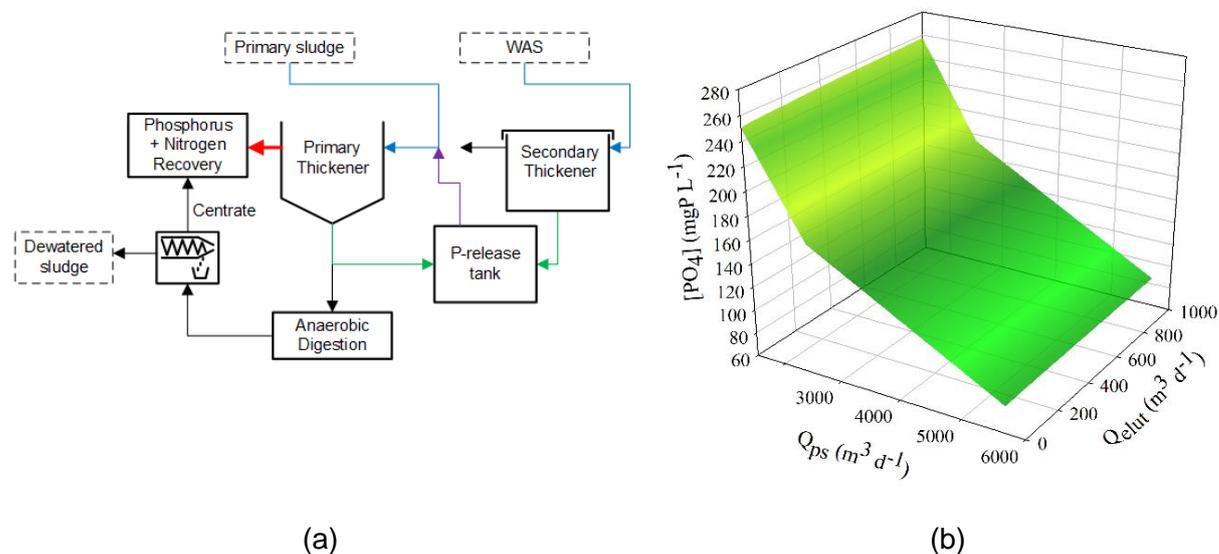


Figure 3: (a) Schematic representation of the sludge line configuration simulated (b) concentration of phosphorus in the primary thickener overflow at different operational conditions: primary sludge flow (Q_{ps}) and elutriation flow (Q_{elut}).

Optimization of an industrial WWTP

Plant-wide models can also be applied to simulate treatment processes of industrial wastewaters. In these cases, the steps of wastewater characterization and parameter calibration take a crucial role. Several complete analytical campaigns are required for wastewater characterization and values from literature cannot be adopted. Model parameter values should be obtained with off-line calibration methodologies to detect bacterial inhibitions. Table 2 shows, as an example, the values obtained for the high influence model parameters in the WWTP of a petrochemical company, quite different from the typical values for urban WWTPs. This showed that wastewater characteristics influence the activity of microorganisms to a large degree.

Table 2: Values of the main model parameters calibrated for the industrial wastewater and the reference ones for sewage

Model parameter	Calibrated	Default
Y_H	0.38	0.63
μ_H (d ⁻¹)	1.04	6
b_H (d ⁻¹)	0.18	0.4
K_F (mg DQO·l ⁻¹)	17.19	4
η_H	0.05	0.43
μ_A (d ⁻¹)	0.2	1
b_A (d ⁻¹)	0.05	0.15
K_{NH} (mg N·l ⁻¹)	0.38	1

Figure 4 shows the oxygen uptake rate values recorded at different substrate concentrations for heterotrophic and autotrophic bacteria. Very high substrate concentrations (higher than usual for urban WWTPs) are required for heterotrophic bacteria to reach their maximum activity. Maximum activity of autotrophic bacteria is relatively low but reached at low ammonium concentrations.

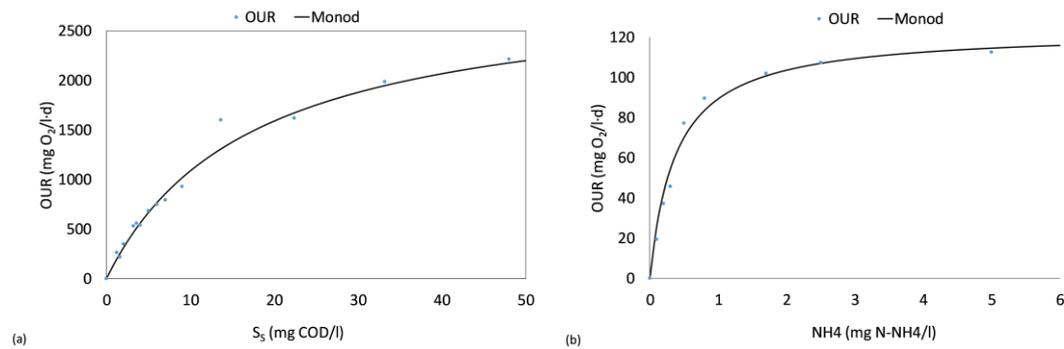


Figure 4. OUR values obtained at different substrate concentrations for a) heterotrophic bacteria b) autotrophic bacteria

Development of control strategies

Control systems design, calibration and validation can be supported by plant-wide models, since it is possible to reproduce the response of the operational units to the performed actions. For instance, plant-wide models allow to take into account the effect of dewatering and supernatant streams recycling to the mainline, affecting virtual nitrogen loading rate. For this, Ruano et al. (2017) used the simulation software DESASS (Ferrer et al., 2008), the IWA Benchmark Simulation Model no. 1 (BSM1) (Alex et al., 2008) as working scenario and the software LoDif Biocontrol[®] (Ferrer et al., 2011) in order to design, calibrate and validate control strategies for optimal nitrogen removal (minimized energy consumption) in activated sludge systems. Figure 5 shows a schematic representation of the development procedure for these controllers to be implemented in full-scale WWTPs.

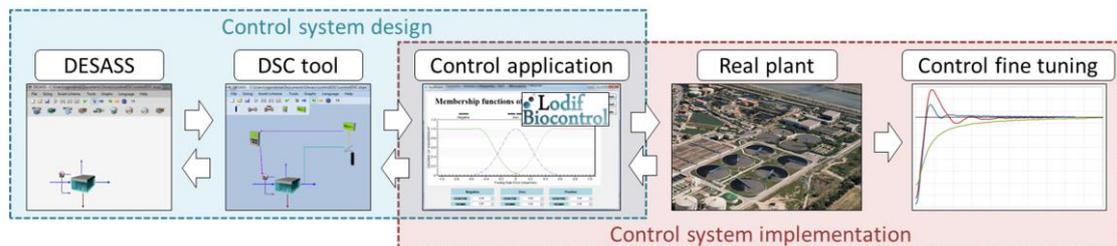


Figure 5: Schematic representation of the development procedure for the controllers to be implemented in WWTPs

An example of simulation results from one of the designs carried out in the study is shown in figure 6. The dissolved oxygen concentration (DO) through a plug-flow reactor was controlled by changing the DO setpoints through time. When the aeration capacity was sufficient, the DO concentration oscillated near the established DO set points. The pattern of the DO set points showed similarities with the dynamics in ammonium concentration, mainly as a result of the information obtained from the pH

sensors that were used to modify the DO set point. Suitable overall process performance was achieved, resulting in enhanced nitrogen removal efficiencies. Moreover, compared to the baseline scenario, the controller reduced significantly the energy demand. Specifically, power requirements were reduced from approx. 0.13 to 0.10 kWh per m³ of treated water.

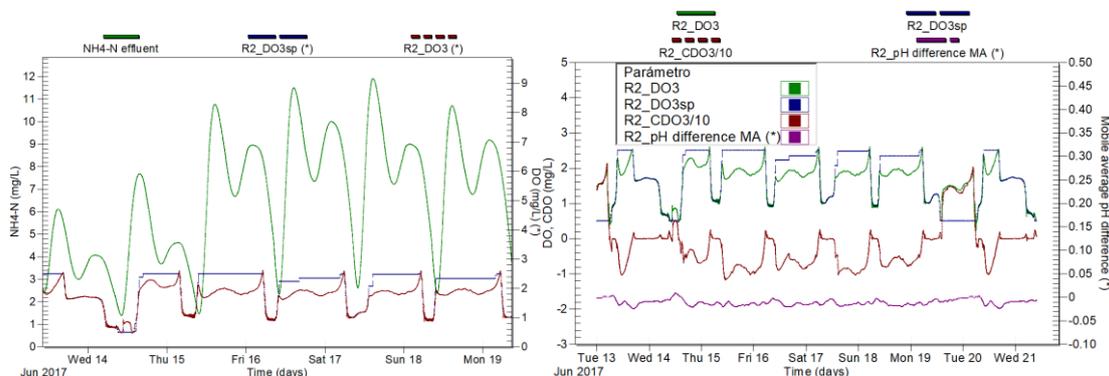


Figure 6: Evolution of: (a) DO set point and ammonium concentration in the outlet of the aerobic reactor; (b) inputs to the controller (pH difference, cumulative DO error, DO and DO set point in last aerated chamber); and (c) WWTP effluent nitrogen content within the different scenarios.

Other extensions for plant wide modelling

A filtration model was also included in the collection model BNRM in order to allow simulation of a wider spectrum of processes. Specifically, a model was proposed for immersed MBRs taking into account the effect of biogas sparging and back-flushing on cake detachment, as well as the risk of irreversible fouling formation. This specific model was validated in an AnMBR system equipped with industrial-scale membranes in the short- (Robles et al., 2013a) and the long-term (Robles et al., 2013b) and used for control purposes, showing that it is possible to efficiently maintain low fouling rates by the application of an upper layer fuzzy-logic controller. In addition, this model was applied to optimise the performance of an AnMBR at pilot scale, obtaining energy savings of up to 25%. A model-based optimization method was also applied to improve the performance of AnMBRs (Robles et al., 2014b; 2018).

Regarding integration of energy and environmental aspects on the modelling target, Pretel et al. (2016a) extended the collection model BNRM with a plant-wide energy model, which was validated in an AnMBR system treating sewage at steady- and unsteady-conditions. The results indicated that the model was capable to reproduce energy variations even when operating at dynamic conditions (*i.e.* variations in ambient temperature and/or inflow temperature). Pretel et al. (2016b) combined this model and life cycle assessment (LCA) for comparing different treatment technologies. In this case, the conclusion could be achieved that an AnMBR combined with a CAS-based post-treatment results in significant reductions in different environmental impact categories mainly due to reduced power requirements.

Summary and future perspectives in wastewater treatment modelling

After the development and widespread of biochemical models to describe separately the most relevant processes in wastewater treatment, the field has evolved in the last decades in the direction of creating plant-wide models that are able to reproduce the

increasing complexity of the plants as a whole. These models take into account a variety of processes such as chemical equilibria, oxygen transfer, greenhouse gas generation, cost, etc. and they intend to be widely and easily applicable. The viability of applying plant-wide model increases with advances in computer technology and the development of simulation platforms. The major role of these plant-wide models and the platforms used for its application in WWTP simulation studies has been shown in this work with a series of case studies.

Remaining challenges in the field of wide-plant modelling are, on the one hand, related to the plant-wide model itself:

i) Further extensions: new processes remain to be considered in these collection models, such as microalgal growth, physical processes for nitrogen components separation (membrane contactors and degassing membranes), autotrophic denitrification using sulfur, bioplastics degradation etc. so that all processes involved can be included in each specific case.

ii) New pollutants: especially in the case that new legal discharge limits are established, (e.g. emerging pollutants or heavy metals). Including these components in a plant-wide model will constitute a great challenge.

On the other hand, achieving a real widespread of plant-wide models among operators of water resource recovery facilities is a current challenge for the scientific community involved in the development of such models. The full potential of plant-wide models for designing new sustainable WRRF, as well as for optimizing existing ones, can only be achieved when these models are transferred to real application.

Regarding model calibration and validation, a consensus should be reached on calibration protocols in order to minimize the variability among model parameters obtained in different studies. For this, the establishment of standardized calibration procedures would be commendable. Data mining from the considerable amount of information currently available on the performance of full-scale implemented processes should also gain importance as a modelling tool in the near future since authors consider that big data in WRRFs is widely underutilized (Newhart et al 2019). In this respect, coupling data-driven modelling methods for plant-wide process monitoring and control with plant-wide models will boost plant-wide optimization (Ge et al., 2017). In addition, integrating computational fluid dynamics models (CFD) with plant-wide models for smarter operation and optimal design remains still a big challenge.

References

Alex, J.,Benedetti, L., Copp, J.,Gernaey,K.V., Jeppsson,U.,Nopens,I., Pons, M.-N., Rieger, L., Rosen, C., Steyer, J.P., Vanrolleghem, P., Winkler, S. (2008) *Benchmark Simulation Model No. 1 (BSM1)*. Division of Industrial Electrical Engineering and Automation, Lund University, Lund, Sweden. <http://www.benchmarkwwtp.org/> (accessed July 2019)

Allison JD, Brown DS, Novo-Gradac KJ. *MINTEQA2/ PRODEFA2, A Geochemical Assessment Model for Environmental Systems: Version 3.0*. Washington, DC.: EPA/600/3- 91/021, USEPA; 1991.

Barat R, Montoya T, Seco A, Ferrer J (2011) Modelling biological and chemically induced precipitation of calcium phosphate in enhanced biological phosphorus removal systems. *Water Research* 45(12), 3744-3752.

Barat R, Serralta J, Ruano MV, Jiménez E, Ribes J, Seco A, Ferrer J (2013) Biological Nutrient Removal Model No. 2 (BNRM2): a general model for wastewater treatment plants. *Water Science and Technology* 67 (7) 1481-1489.

Batstone DJ, Keller J, Angelidaki I, Kalyuzhnyi SV, Pavlostathis SG, Rozzi A, Sanders WTM, Siegrist H, Vavilin VA (2002) *Anaerobic Digestion Model No.1*. IWA STR No.13 London, UK: IWA Publishing.

Batstone, D.J., Hülsen, T., Mehta, C.M., Keller, J. (2015) Platforms for energy and nutrient recovery from domestic wastewater: A review. *Chemosphere* 140, 2–11.

Borrás Falomir L (2008). *Técnicas microbiológicas aplicadas a la identificación y cuantificación de organismos presentes en sistemas EBPR (Microbiological techniques applied to identification and quantification of organisms present in EBPR Systems)*. PhD Thesis, Universitat Politècnica de València, Valencia, Spain.

Claros J, Jiménez E, Aguado D, Ferrer J, Seco A, Serralta J (2011) Effect of pH and HNO₂ concentration on the activity of ammonia-oxidizing bacteria in a partial nitrification reactor. *Water Science and Technology* 67(11), 2587-2594.

Copp, J.B. (2002) *The COST Simulation Benchmark – Description and Simulator Manual*. Office for Official Publications of the European Communities, Luxembourg.

Copp JB, Jeppsson U, Rosen C (2003) Towards an ASM1 - ADM1 State Variable Interface for Plant-Wide Wastewater Treatment Modeling. In: *proceedings of the Water Environment Federation Conference (WEFTEC2003)*, 11th – 15th November 2003, Los Angeles, California (United States)

Durán F (2013) *Modelación matemática del tratamiento anaerobio de aguas residuales urbanas incluyendo las bacterias sulfatorreductoras. Aplicación a un biorreactor anaerobio de membranas (Mathematical model of urban wastewater anaerobic treatment including sulphate reducing bacteria. Application to an Anaerobic Membrane Bioreactor)*. PhD Thesis, Universitat Politècnica de València, Valencia, Spain.

Durán F, Robles A, Seco A, Ferrer J, Ribes J, Serralta J (2017) *Modelling the anaerobic treatment of urban wastewater: application to AnMBR technology*. 15th IWA World Conference on Anaerobic Digestion. 17th-20th October, Beijing (China).

Ekama GA (2009) Using bioprocess stoichiometry to build a plant-wide mass balance based steady-state WWTP model. *Water Research* 43, 2101-2120.

EPA. User's manual version 4.03 2006. <https://www.epa.gov/ceam/minteqa2-equilibrium-speciation-model>. (accessed July 2019).

- Fernández-Arévalo T, Lizarralde I, Fdz-Polanco F, Pérez-Elvira SI, Garrido JM, Puig S, Poch M, Grau P, Ayesa E (2017) Quantitative assessment of energy and resource recovery in wastewater treatment plants based on plant-wide simulations. *Water Research* 118, 272-288.
- Ferrer J, Seco A, Serralta J, Ribes J, Manga J, Asensi E, Morenilla JJ, Llavador F (2008) DESASS - A software tool for designing, simulating and optimising WWTPs. *Environmental Modelling and Software* 23, 19-26.
- Ferrer J., Seco A., Ruano M.V., Ribes J., Serralta J., Gómez T., Robles A. (2011) *LoDif BioControl® control software*, intellectual property. Main Institution: Universitat de València; Universitat Politècnica de València.
- Flores-Alsina X, Corominas L, Snip L, Vanrolleghem PA (2011) Including greenhouse gas emissions during benchmarking of wastewater treatment plant control strategies. *Water Research* 45(16), 4700-4710.
- Flores-Alsina X, M. Arnell, Y. Amerlinck, L. Corominas, K.V. Gernaey, L. Guo, E. Lindblom, I. Nopens, J. Porro, A. Shaw, L. Snip, P.A. Vanrolleghem, U. Jeppsson (2013) Balancing effluent quality, economic cost and greenhouse gas emissions during the evaluation of (plant-wide) control/operational strategies in WWTPs. *Science of the Total Environment* 466-467, 616-624.
- Flores-Alsina X, Kazadi Mbamba C, Solon K, Vrecko D, Tait S, Batston DJ, Jeppsson U, Gernaey K (2015) A plant-wide aqueous phase chemistry module describing pH variations and ion speciation/pairing in wastewater treatment process models. *Water Research* 85, 255-265.
- Ge Z. (2017) Review on data-driven modeling and monitoring for plant-wide industrial processes. *Chemometrics and Intelligent Laboratory Systems* 171 (2017) 16–25
- Grau P, de Gracia M, Vanrolleghem PA, Ayesa E (2007) A new plant-wide modelling methodology for WWTPs. *Water Research* 41, 4357-4372.
- Grau P, Copp J, Vanrolleghem PA, Takacs I, Ayesa E (2009) A comparative analysis of different approaches for integrated WWTP modelling. *Water Science and Technology* 59(1), 141-147.
- Henze, Gujer W, Mino T, van Loosdrecht MCM (2000) *Activated Sludge Models ASM1, ASM2, ASM2d and ASM3*. IWA Scientific and Technical Report No.9, London, UK: IWA Publishing.
- Jeppsson, U., Pons, M.N. (2004) The COST benchmark simulation model - current state and future perspective. *Control Engineering Practice* 12 (3), 299-304.
- Jeppsson U, Rosen C, Alex J, Copp J, Gernaey KV, Pons M-N, Vanrolleghem PA (2006) Towards a benchmark simulation model for plant-wide control strategy performance evaluation of WWTPs. *Water Science and Technology* 53(1), 287-295.
- Jeppsson U, Pons MN, Nopens I, Alex J, Coop J, Gernaey KV, Rosen C, Steyer JP, Vanrolleghem PA (2007) Benchmark Simulation Model No.2-General Protocol and exploratory case studies. *Water Science and Technology* 56(8),67-78.

Jiménez Douglas E (2010) *Modelación matemática del proceso de nitrificación en dos etapas. Desarrollo de metodologías de calibración del modelo para un reactor SHARON y un proceso de fangos activados (Mathematical modeling of two-step nitrification process. Development of calibration methodologies for the model in a SHARON reactor and in an Activated Sludge process)* PhD Thesis, Universitat Politècnica de València, Valencia, Spain.

Jiménez E, Giménez JB, Ruano MV, Ferrer J, Serralta J (2011) Effect of pH and nitrite concentration on nitrite oxidation rate. *Bioresource Technology* 102 (19) 8741-8747.

Jiménez E, Giménez JB, Seco A, Ferrer J, Serralta J (2012) Effect of pH, substrate and free nitrous acid concentrations on ammonium oxidation rate. *Bioresource Technology* 124, 478-484.

Jones R.M., Takács. I. (2004) *Importance of anaerobic digestion modelling on predicting waste-water treatment plants*. Proceedings of Anaerobic Digestion 2004, 10th World Congress, Montreal, Canada, 24 Aug-2Sep, 2004, pp. 1371-1375.

Kazadi Mbamba C, Flores-Alsina X, Batstone DJ, Tait S (2016) Validation of a plant-wide phosphorus modelling approach with minerals precipitation in a full-scale WWTP. *Water Research* 100, 169-183.

C. Kazadi Mbamba, E. Lindblom, X. Flores-Alsina, S. Tait, S. Anderson, R. Saagi, D.J. Batstone, K.V. Gernaey, U. Jeppsson (2019) Plant-wide model-based analysis of iron dosage strategies for chemical phosphorus removal in wastewater treatment systems. *Water Research* 155, 12-25.

Lizarralde I, Fernández-Arévalo T, Brouckaert C, Vanrolleghem P, Ikumi DS, Ekama GA, Ayesa E, Grau P (2015) A new general methodology for incorporating physico-chemical transformations into multiphase wastewater treatment process models. *Water Research* 74, 239-256.

Lizarralde I, Fernández-Arévalo T, Manas A, Ayesa E, Grau P (2019) Model-based optimization of phosphorus management strategies in Sur WWTP, Madrid. *Water Research* 153, 39-52.

Lopez-Vazquez CM, Oehmen A, Hooijmans CM, Brdjanovic D, Gijzen HJ, Yuan Z, van Loosdrecht MC (2009) Modeling the PAO-GAO competition: effects of carbon source, pH and temperature. *Water Research* 43(2), 450-462.

Maere T, Verrecht B, Moerenhout S, Judd S, Nopens I (2011) BSM-MBR: A benchmark simulation model to compare control and operational strategies for membrane bioreactors. *Water Research* 45, 2181-2190.

Mannina G, Ekama G, Caniani D, Cosenza A, Esposito G, Gori R, Garrido-Baserba M, Rosso D, Olsson G (2016) Greenhouse gases from wastewater treatment—A review of modelling tools. *Science of The Total Environment* 551–552, 254-270.

- Mannina G, Ferreira Rebouças T, Cosenza A, Chandran K (2019) A plant-wide wastewater treatment plant model for carbon and energy footprint: Model application and scenario analysis. *Journal of Cleaner Production* 217, 244-256.
- Marti N, Barat R, Seco A, Pastor L, Bouzas A (2017) Sludge management modeling to enhance P-recovery as struvite in wastewater treatment plants. *Journal of Environmental Management* 196, 340-346.
- Newhart KB, Holloway RW, Hering AS, Cath TY (2019) Data-driven performance analyses of wastewater treatment plants: A review. *Water Research* 157, 498-513.
- Nopens I, Batstone D, Copp JB, Jeppsson U, Volcke EIP, Alex J, Vanrolleghem PA (2009) A practical ASM/ADM model interface for enhanced dynamic plantwide simulation. *Water Research* 43: 1913-1923.
- Nopens, I., Benedetti, L., Jeppsson, U., Pons, M.N., Alex, J., Copp, J.B., Gernaey, K.V., Rosen, C., Steyer, J.P., Vanrolleghem, P.A., 2010. Benchmark Simulation Model No 2: finalisation of plant layout and default control strategy. *Water Science and Technology* 62(9), 1967-1974.
- Penya-Roja J. M., Seco A., Ferrer J., Serralta J. (2002) Calibration and Validation of Activated Sludge Model No.2d for Spanish Municipal Wastewater. *Environmental Technology* 23, 849-862.
- Pretel, R., Robles, A., Ruano, M.V., Seco, A., Ferrer, J., 2016a. A plant-wide energy model for wastewater treatment plants: application to anaerobic membrane bioreactor technology. *Environmental Technology* 37, 2298–2315.
- Pretel, R., Robles, A., Ruano, M.V., Seco, A., Ferrer, J., 2016b. Economic and environmental sustainability of submerged anaerobic MBR-based (AnMBR-based) technology as compared to aerobic-based technologies for moderate-/high-loaded urban wastewater treatment. *Journal of Environmental Management* 166, 45–54.
- Rehman, U., Audenaert, W., Amerlinck, Y., Maere, T., Arnaldos, M., Nopens, I. (2017) How well-mixed is well mixed? Hydrodynamic-biokinetic model integration in an aerated tank of a full-scale water resource recovery facility. *Water Science & Technology* 76(8), 1950–1965.
- Robles, A., Ruano, M.V., Ribes, J., Seco, A., Ferrer, J., 2013a. A filtration model applied to submerged anaerobic MBRs (SAnMBRs). *Journal of Membrane Science* 444, 139–147.
- Robles, A., Ruano, M.V., Ribes, J., Seco, A., Ferrer, J., 2013b. Mathematical modelling of filtration in submerged anaerobic MBRs (SAnMBRs): Long-term validation. *Journal of Membrane Science* 446, 303–309.
- Robles, A., Ruano, M.V., Ribes, J., Seco, A., Ferrer, J., 2014b. Model-based automatic tuning of a filtration control system for submerged anaerobic membrane bioreactors (AnMBR). *Journal of Membrane Science* 465, 14–26.

Robles A, Capson-Tojo G, Ruano MV, Seco A, Ferrer J (2018) Real-time optimization of the key filtration parameters in an AnMBR: Urban wastewater mono-digestion vs. co-digestion with domestic food waste. *Waste Management* 80, 299-309.

Rosen, C., Jeppsson, U., Vanrolleghem, P.A., 2004. Towards a common benchmark for long-term process control and monitoring performance evaluation. *Water Science and Technology* 50(11), 41-49.

Ruano MV, Serralta J, Ribes J, Garcia-Usach F, Bouzas A, Barat R, Seco A, Ferrer J (2012) Application of the general model 'Biological Nutrient Removal Model No. 1' to upgrade two full-scale WWTPs. *Environmental Technology* 33, 1005-1012.

Ruano MV, Robles A, Seco A, Ferrer J and Ribes J (2017) *Benchmarking of control strategies implemented in a dedicated control platform for wastewater treatment processes*. 12th IWA Specialized Conference on Instrumentation, Control and Automation, ICA 2017, 11th-14th June 2017, Quebec (Canada).

Seco A, Ribes J, Serralta J, Ferrer J (2004) Biological Nutrient Removal Model No. 1 (BNRM1). *Water Science and Technology* 50 (6) 69-78.

Seco A, Ribes J, Serralta J, Ferrer J. *Upgrading the Denia WWTP according to BNRMI simulations*. I IWA Specialized Conference: Nutrient Management in Wastewater Treatment Processes and Recycle Streams. 19th September 2005, Krakow (Poland)

Serralta J, Ferrer J, Borrás L, Seco A (2004) An extension of ASM2d including pH calculation. *Water Research* 38, 4029–4038

Solon K, Flores-Alsina X, Kazadi Mbamba C, Ikumi D, Volcke EIP, Vaneckhaute C, Ekama G, Vanrolleghem PA, Batstone DJ, Gernaey KV, Jeppsson U (2017) Plant-wide modelling of phosphorus transformations in wastewater treatment systems: Impacts of control and operational strategies. *Water Research* 113, 97-110.

Solon K, Jia M, EIP Volcke (2019a) Process schemes for future energy-positive water resource recovery facilities. *Water Science and Technology* 79(7), 1808-1820.

Solon K, Jia M, Volcke EIP, Spérandio M, Van Loosdrecht MCM (2019b) Resource recovery and wastewater treatment modelling. *Environmental Science: Water Research and Technology* 5, 631-642.

Vanrolleghem PA, Rosen C, Zaher U, Copp J, Benedetti L, Ayesa E, Jeppsson U (2005) Continuity based interfacing of models for wastewater systems described by Peterson matrices. *Water Science and Technology* 52 (1-2): 149-500.